

# NASA Technical Memorandum 83281

NASA-TM-83281 19820015320

AN ACCURATE METHOD FOR EVALUATING THE KERNEL  
OF THE INTEGRAL EQUATION RELATING LIFT TO  
DOWNWASH IN UNSTEADY POTENTIAL FLOW

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APRIL 1982

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# AN ACCURATE AND EFFICIENT METHOD FOR EVALUATING THE KERNEL OF THE INTEGRAL EQUATION RELATING PRESSURE TO NORMALWASH IN UNSTEADY POTENTIAL FLOW

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## SUMMARY

This paper describes an accurate economical method for generating approximations to the kernel of the integral equation relating unsteady pressure to normalwash in nonplanar flow. The method is capable of generating approximations of arbitrary accuracy. It is based on approximating the algebraic part of the non elementary integrals in the kernel by exponential functions and then integrating termwise. The exponent spacing in the approximation is a geometric sequence. The coefficients and exponent multiplier of the exponential approximation are computed by least squares so the method is completely automated. Exponential approximates generated in this manner are two orders of magnitude more accurate than the exponential approximation that is currently most often used for this purpose. Coefficients for 8, 12, 24, and 72 term approximations are tabulated in the report. Also, since the method is automated, it can be used to generate approximations to attain any desired trade-off between accuracy and computing cost.

## NOMENCLATURE

$a_k$	coefficient in exponential approximation
$b$	exponent multiplier in exponential approximation
$b_k$	exponent in exponential approximation
$c_{jk}$	element of matrix of least squares normal equations
$d_j$	elements of right-hand-side vector of normal equations
$E(b)$	least squares penalty function
$E(t)$	error in $f(t)$ , $g(t) - f(t)$
$E(s,r)$	error in $F(s,r)$ , $\int_s^\infty e^{-irt} [g(t) - f(t)] dt$
$f(t)$	function to be approximated, equation (12)
$F(s,r)$	Computational form of incomplete modified Struve function occurring in planar part of kernel
$\bar{F}(s,r)$	Incomplete modified Struve function occurring in planar part of kernel

$g(t)$	an approximation to $f(t)$
$G(s,r)$	Computational form of incomplete modified Struve function occurring in nonplanar part of kernel
$\bar{G}(s,r)$	Incomplete modified Struve function occurring in nonplanar part of kernel
$p_k$	exponent coefficient in equation (A2). In this paper either $p_k = k$ or $p_k = 2^k/m$ .
$r$	Frequency term occurring in argument of exponential factor ( $r = (\omega/U) \cdot \sqrt{(y_0^2 + z_0^2)}$ times the variable of integration of equations (6) and (7))
$s$	Lower limit of integration ( $s = s_1/\sqrt{(y_0^2 + z_0^2)}$ )
$t$	variable of integration in definition of $F(s,r)$ and $G(s,r)$

The symbols occurring in equations (1) thru (7) not defined above are defined in the references. They are not used elsewhere in the paper. Equations (1) thru (7) merely illustrate a use for  $F(s,r)$  and  $G(s,r)$ .

## INTRODUCTION

This paper describes a method for computing two incomplete modified Struve functions that occur in unsteady aerodynamics. These two functions are the nonelementary part of the unsteady kernel of the integral equation relating lift to downwash in three dimensional potential flow.

The incomplete Struve functions approximated in this report occur whenever one attempts to compute the three dimensional velocity field induced by unsteady doublet distributions. The most common occurrence is when evaluating the acceleration potential kernel of the downwash integral equation as in reference 1. However, the same Struve functions occur even if the velocity potential is used, although the kernel is very different. For example, a 24 term approximation developed herein is used to compute the wake contribution in a velocity potential program called SOUSSA (reference 2).

The method developed in this paper is the familiar technique of replacing the algebraic factor in the defining integral by an exponential approximation and then evaluating the integral in closed form. The new exponential approximations described in this paper have coefficients computed by an easily automated least squares process and hence can be used to approximate the incomplete Struve functions to any desired accuracy.

The paper explains the reason for using exponential approximations instead of series expansions or direct numerical integration. It also surveys several previously published approximations and assesses their accuracy.

Coefficients for four new approximations are tabulated in the paper. The least squares process is explained in sufficient detail to enable the reader to generate his own approximations to fit the accuracy or computing time constraints of his problem.

#### STATEMENT OF PROBLEM

Consider the integral equation relating unsteady pressure to normalwash in three dimensional potential flow

$$w(x, s) = \frac{1}{(8\pi)} \left( \sum_{n=1}^N \iint_{S_n} K(x, \xi; s, \sigma; \omega/U, M) p(\xi, \sigma) d\xi d\sigma \right) \quad (1)$$

A convenient representation of the kernel,  $K$ , above is the one given by Harder and Rodden (reference 3)

$$K = \exp(-i\omega x_0/U) (K_1 T_1/r^2 + K_2 T_2/r^4) \quad (2)$$

where  $x_0$  is the distance in the free stream direction between the sending and receiving points and

$$T_1 = \cos(\gamma_r - \gamma_s) \quad (3)$$

$$T_2 = (z_0 \cos \gamma_r - y_0 \sin \gamma_r)(z_0 \cos \gamma_s - y_0 \sin \gamma_s) \quad (4)$$

$$r = (y_0^2 + z_0^2)^{1/2} \quad (5)$$

where  $y_0$  and  $z_0$  are the distance from sending to receiving points measured normal to the freestream and  $\gamma_r, \gamma_s$  are dihedral angles.

$$K_1 = -u(x_0 - Br) \left\{ \frac{Mr^2}{R} \left[ \frac{\exp(-i\omega s_2/U)}{(r^2 + s_2^2)^{1/2}} + \frac{\exp(-i\omega s_1/U)}{(r^2 + s_1^2)^{1/2}} \right] + \int_{s_1}^{s_2} \frac{r^2 \exp(i\omega s/U)}{(r^2 + s^2)^{3/2}} ds \right\} \quad (6)$$

$$K_2 = u(x_0 - Br) \left\{ \frac{Mr^4 \exp(-i\omega s_2/U)}{R(r^2 + s_2^2)^{3/2}} \right.$$

$$\cdot \left[ 2 - \frac{B^2(r^2 + s_2^2)}{R^2} - \frac{Ms_2}{R} \right]$$

$$-i \frac{M^2 r^3 (\omega r/U) \exp(i\omega s_2/U)}{R^2 (r^2 + s_2^2)^{1/2}}$$

$$+ \frac{Mr^4 \exp(-i\omega s_1/U)}{R(r^2 + s_1^2)^{3/2}} \left[ 2 - \frac{B^2(r^2 + s_1^2)}{R^2} + \frac{Ms_1}{R} \right]$$

$$+ i \frac{M^2 r^3 (\omega r/U) \exp(-i\omega s_1/U)}{R^2 (r^2 + s_1^2)^{1/2}}$$

$$+ 3 \int_{s_1}^{s_2} \frac{r^4 \exp(i\omega s/U)}{(r^2 + s^2)^{5/2}} ds \quad (7)$$

The unit function,  $u(x)$ , in equation (6) is one if  $x > 0$  and is zero if  $x < 0$ . The only non elementary terms in the above expressions for  $K_1$  and  $K_2$  are the integrals. They can be rescaled to

$$F(s, r) = \int_s^\infty e^{-irt} (1 + t^2)^{-3/2} dt \quad (8)$$

and

$$\bar{G}(s, r) = \int_s^\infty e^{-irt} (1 + t^2)^{-5/2} dt \quad (9)$$

These integrals are called incomplete modified Struve functions. In subsonic flow the upper limit of integration is infinity as in equations (8) and (9) above. In supersonic flow the upper limit is variable so the integrals in equations (6) and (7) are expressed as differences of incomplete Struve functions. The algebraic part of equations (8) or (9) could be approximated by an exponential function. However, to facilitate comparison with other exponential approximations the exponential approximations were used in the integrals

$$F(s, r) = \int_s^\infty e^{-irt} \left( 1 - \frac{t}{\sqrt{1+t^2}} \right) dt \quad (10)$$

and

$$G(s,r) = \int_s^{\infty} e^{-irt} t(1 - \frac{t}{\sqrt{1+t^2}}) dt \quad (11)$$

that are related to  $F$  and  $G$  by integration by parts (see reference 4 for details of the integration by parts). The function to be approximated by exponential approximations is

$$f(t) = 1 - t/\sqrt{1+t^2} \quad (12)$$

The exponential approximations are

$$g(t) = \sum_{k=1}^n a_k \exp(-b_k t) \quad (13)$$

This reduces the evaluation of  $F$  and  $G$  to the evaluation of elementary integrals. Equation (13) can only be used if  $t$  is non-negative. If  $t$  is negative then  $g(t) = 2 - g(|t|)$ .

Replacing  $f(t)$  by an exponential approximation is not the only way to evaluate  $F(s,r)$  and  $G(s,r)$ . Before electing to use this method several other techniques were investigated in some detail. Direct numerical integration was found to be too expensive. A series expansion of one or the other integral factor followed by a closed form integration is economical; but every such expansion has a very limited area of application in the  $s$ - $r$  plane. To evaluate  $F(s,r)$  by a combination of an asymptotic series for large  $s$  (obtained by iterated integration by parts) and closed form integration of various series expansions of  $\exp(-irt)$  and  $t/\sqrt{1+t^2}$  would take at least half a dozen different algorithms. This would result in a computer subprogram that, while inexpensive to use, would be very expensive to develop, certify, and maintain.

For the reasons stated above, exponential approximations having the form shown in equation (13) are the most commonly used method for evaluating the integrals  $F(s,r)$  and  $G(s,r)$ . In the next section several currently used approximations are discussed.

#### A SURVEY OF PREVIOUS EXPONENTIAL APPROXIMATIONS

There are two reasons for surveying previous exponential approximations to  $f(t)$ . One, of course, is to point out their deficiencies to justify developing a new family of approximations. A more important reason is to show how they contributed to the development of the least squares method described herein and to show which features of previous methods have been retained.

The first use of an exponential approximation to  $f(t)$  to evaluate the integral  $F(s,r)$  was by Watkins, Woolston, and Cunningham (reference 1). They used the approximation

$$g(t) = \sum_{k=1}^4 a_k \exp(-b_k t) \quad (14)$$

where the  $a_k, b_k$  are tabulated below:

$$\begin{aligned} a_1 &= .101 \\ a_2 &= .899 \\ a_3 &= .0047404665 \text{ i} \\ a_4 &= -.0047404665 \text{ i} \\ b_1 &= .329 \\ b_2 &= 1.4067 \\ b_3 &= 2.9 + 3.1415926 \text{ i} \\ b_4 &= 2.9 - 3.1415926 \text{ i} \end{aligned} \quad (15)$$

This approximation will be referred to as W4 (Watkins, 4 term). The error in this approximation to  $f(t)$ , that is  $e(t) = g(t) - f(t)$ , is plotted as short dashes in Figure 1.

The approximation W4 was derived long before the ready availability of high speed computing machinery. The coefficients,  $a(k)$ , and exponents,  $b(k)$ , were generated as follows:

1. A large scale plot of the function  $f(t) = 1-t/\sqrt{1+t^2}$  was constructed on graph paper.
2. Several plots of  $a \exp(-bt)$  for different values of  $a$  and  $b$  were drawn on the same sheet of paper. Eventually, by trial and error, an  $a, b$  were found that appeared to give a best fit.
3. The difference between the function being fitted,  $f(t)$ , and the approximation  $a \exp(-bt)$  was drawn on a large scale plot.
4. Steps 2 and 3 above were repeated several times, using successive difference plots, to give an exponential series with several terms.

A more commonly used approximation to  $f(t)$  is the 11 term exponential polynomial

$$g(t) = \sum_{k=1}^{11} a_k e^{-b_k t} \quad (16)$$

due to Laschka (reference 5). The exponent,  $b$ , and the coefficients,  $a_k$ , appearing in this approximation are tabulated below:

$$\begin{aligned} b &= .372 \\ a_1 &= .24186198 \\ a_2 &= -2.7918027 \\ a_3 &= 24.991079 \\ a_4 &= -111.59196 \\ a_5 &= 271.43549 \\ a_6 &= -305.75288 \\ a_7 &= 41.1836 \\ a_8 &= 545.98537 \\ a_9 &= -644.78155 \\ a_{10} &= 328.72755 \\ a_{11} &= -64.279511 \end{aligned} \quad (17)$$

This approximation will be referred to as L11. In L11, instead of 11 unrelated exponents  $b_k$ , there is a single exponent,  $b$ , and its multiples. This means that even though L11 has many more terms than W4 the integral  $F(s,r)$  can be evaluated almost as fast using L11 as using W4 because only a single exponential function has to be evaluated. Figure 1 (long dashes) also shows that L11 is more accurate than W4. The computer code to approximate the integral  $F(s,r)$  is somewhat easier to write using the approximation L11 than it is using the approximation W4. This is probably why the approximation L11 is so widely used.

Reference 5 does not state how the exponent,  $b$ , or the coefficients,  $a_k$ , in L11 were computed. Inspection of Figure 1 leads one to suspect that they were computed in essentially the same manner as the coefficients and exponents of W4. There are 12 free parameters in this approximation, 1 exponent and 11 coefficients. If they had been computed by some sort of systematic optimization procedures such as least squares or minimax then the number of nodes (points where  $e(t) = 0$ ) on the error plot, Figure 1, would approximately equal the number of free parameters.

The approximation D11 has been in use for several years in a computer program based on reference 1 but the coefficients have not been published. It has the same form as L11, namely equation (16). However the coefficients and exponent were computed to minimize the integrated square error

$$E = \int_0^{\infty} w(t) (g(t) - f(t))^2 dt \quad (18)$$

using the weight function  $w(t) = t^{-1/2}$ . The reason for this choice will be discussed later. The exponent and coefficients for D11 are tabulated below:

$b = .1539$   
 $a_1 = .0545$   
 $a_2 = -.8049$   
 $a_3 = 6.3712$   
 $a_4 = -10.8582$   
 $a_5 = -130.6866$   
 $a_6 = 915.2209$   
 $a_7 = -2793.8215$   
 $a_8 = 4800.8897$   
 $a_9 = -4792.6556$   
 $a_{10} = 2596.7163$   
 $a_{11} = -590.2260$

The least squares procedure used to generate D11 was very easy to implement because there is only one non-linear parameter,  $b$ . The form of the approximation L11 was chosen to minimize the execution time of the computed approximation but it also makes the coefficients in the approximation easier to compute.

Figure 1 (solid curve) indicates that D11 is much more accurate than L11. Since it has the same form as L11 a program that uses L11 can be converted to one using D11 by only changing one or two data statements. This similarity in

form is the only reason for tabulating the D11 coefficients because it will be shown later that much more accurate approximations can be obtained by changing the expression for the exponents  $b_k$  to something other than  $k \cdot b$ . Before considering this, however, it's instructive to see what happens to an approximation such as D11 when the number of terms,  $n$  is increased.

Consider the approximation

$$g(t) = \sum_{k=1}^n a_k e^{-kbt} \quad (20)$$

where the exponent  $b$  and the coefficient  $a_k$  are chosen to minimize the integral  $E$  of equation (18). Figure 2 shows the  $e(t)$  vs.  $t$  plots for three of these approximations. For the three approximations shown the maximum error decreases with  $n$  as expected. The ragged behavior of the 24 term approximation for  $t$  near zero is due to cancellation errors. The coefficients  $a_k$  are very large while both the function being approximated  $f(t)$  and the approximation functions  $\exp(-kbt)$  are near unity. For  $n$  slightly greater than 24 this cancellation due to large coefficients becomes the main source of error in these approximations and no further gain in accuracy is attainable using  $b_k = k \cdot b$  unless the computer word length is increased.

The solution to this cancellation error problem is suggested by an exponential approximation due to Jordan (ref. 6). The  $e(t)$  vs.  $t$  plot for this approximation, called J10, is shown as the solid curve in Figure 3.

This approximation is of the form

$$g(t) = a_0 \exp(-b_0 t) + \sum_{k=1}^9 a_k e^{-2^k b t} \quad (21)$$

with exponents and coefficients tabulated below:

$b_0 = 3$   
 $a_0 = .7048426$   
 $b = .0625$   
 $a_1 = .002907843$   
 $a_2 = .002591528$   
 $a_3 = .02667074$   
 $a_4 = .070971$   
 $a_5 = .347837$   
 $a_6 = .5556069$   
 $a_7 = -.776979$   
 $a_8 = .07004561$   
 $a_9 = -.004557519$  (22)

Although the exponents  $b_k$  in this approximation are somewhat more complicated than in L11 or D11, the sum in equation (21), when substituted into the integral  $F(s,r)$ , can still be evaluated without repeated calls to the exponentiation subprogram. This simplification occurs because  $\exp(-2^k b t)$  is equal to  $(\exp(-2^{k-1} b t))^2$  so that the exponential functions can be computed recursively as in L11.

The approximation J10 is much more accurate than L11 and is somewhat more accurate than

D11. It would take a 15 term approximation similar to D11 to attain the accuracy of J10. However it isn't the accuracy of J10 that is important. It is the fact that the coefficients,  $a_k$ , in J10 are all bounded by unity so cancellation errors are very small.

Reference 6, like reference 1 and 5, does not state how the exponents and coefficients were computed. The coefficients in J10 were probably computed in a manner similar to that used for the W4 coefficients. This is indicated by the fact that the number of nodes shown in figure 3 (eight) is much less than the number of free parameters (twelve). By contrast, the approximations D8.1 and D12.1, developed using the methods of the next section, and also plotted in figure 3, have the same number of nodes as free parameters.

#### EXPONENTIAL APPROXIMATIONS OF ARBITRARY ACCURACY

In this section a family of new exponential approximations of the form

$$g(t) = \sum_{k=1}^n a_k \exp(2^k/bt) \quad (23)$$

will be investigated. For each of these approximation the exponent  $b$  and the coefficients  $a_k$  were computed to minimize the integral  $E$  of equation (18). The coefficients  $a_k$  enter into the error minimization process linearly and the exponent  $b$  enters nonlinearly. As a consequence, for each value of  $n$  and  $m$  there are several values of  $b$  for which  $E$  is a relative minimum. Of these relative minima the value of  $b$  chosen was not the value which minimized  $E$  in the absolute sense but rather, the values that minimized the maximum values of  $|e(t)| = |g(t) - f(t)|$ .

Exponents and coefficients for four of these approximations, designated D8.1, D12.1, D24.2, and D72.3 ( $D_{n,m}$ ) are tabulated in TABLE I. The error  $e(t)$  in D8.1 and D12.1 is also plotted in Figure 3. A summary of some of the properties of these approximations is listed in TABLE II. Properties of the approximations discussed previously are also included in TABLE II.

Approximations D8.1 and D12.1 can be used to rapidly evaluate the integral  $F(s,r)$ . The execution times (TABLE II) are comparable to those of approximations, W4, L11/D11, and J10. However D8.1 and D12.1 are much more accurate. The author knows of no study to determine how accurately the integral  $F(s,r)$  has to be computed for various aeroelastic applications. Approximation D24.2 permits computing the integral  $F(s,r)$  to about 3.5 more significant figures than D12.1. This is about full register accuracy on a short word length computer. Approximation D72.2 is probably more accurate than is needed for any engineering purpose. These coefficients are included because they were used to assess the error of the other approximations.

The form of the expression chosen for the exponents, namely

$$b_k = 2^{k/m} b \quad (24)$$

was dictated to a large extent by the approximations discussed in the previous section. In L11 the form  $k \cdot b$  was introduced to reduce the number of exponential function evaluations that occurred when evaluating  $F(s,r)$ . However this choice also reduced the number of nonlinear parameters in the least squares error minimization process used to generate D11. This made it possible to automate the process. The choice,  $b_k = 2^{k/m} b$ , suggested by J10, is almost as good as that of D11 for convenience in computing the integral  $F(s,r)$  and is better for the least squares process. This is because the matrix of the normal equations has a much lower condition number when  $2^{k/m} b$  is used than it has when  $k \cdot b$  is used.

The choice,  $b_k = 2^{k/m} b$ , corresponding to  $m = 1$  in equation (23), was used to generate the approximation D8.1 and D12.1. However when an attempt was made to generate D24.1 this way the result was only slightly more accurate than D12.1. The exponent,  $b$  enters into the least squares process in a nonlinear manner so there is more than one value of  $b$  for which  $E = E(b)$  is a relative minimum. When  $n$  is 12 there are eight of these relative minima and the lowest value of  $E$  is  $1.56E-9$ . Increasing  $n$  to 24 increases the number of relative minima to twenty but only reduces the lowest value of  $E$  to  $9.07E-10$ . In fact, when  $n$  is 24 there are ten relative minima with integrated square errors,  $E$ , between  $9.07E-10$  and  $9.9E-10$ . As  $n$  increases a value of  $n$  is reached for which increasing  $n$  increases the number of relative minima without decreasing the value of  $E$  at the lowest relative minimum. This happens because when  $n$  is increased from 12 to 24 the value of  $b$  was rescaled so that effectively the additional  $b_k$  were all inserted ahead of  $b_1$ , where their effect was to reduce the  $|e(t)|$  for  $t$  near zero, and they were also inserted after  $b_{12}$ , where their effect was to reduce  $|e(t)|$  for  $t$  very large. None of them were interpolated between the  $b_k$  to reduce  $|e(t)|$  in the middle of its range. Changing  $b_k$  from  $2^{k/m} b$  to  $2^{k/2} b$  has the desired effect of reducing  $|e(t)|$  in the middle of its range. When  $n$  is set to 24 and  $m$  is set to 2 only seven relative minima are obtained and the value of  $E$  at the lowest is  $1.78E-12$ , a significant improvement over  $m = 1$ . One might think that since  $m = 2$  is an improvement when  $n = 24$ , that  $m = 3$  would be even better. When  $m$  was set to 3 the number of relative minima was reduced to four but the lowest value of  $E$  was increased to  $1.9E-10$ . Also for  $n = 24$  and  $m = 3$  the coefficients  $a_k$  were very large so some cancellation errors can occur. For most values of  $n$  there is a single optimum value of  $m$ . If there are two optimum values of  $m$  for a particular value of  $n$  then the lower should be chosen because evaluating  $F(s,r)$  requires  $m$  exponential function evaluations.

Exponential approximations of the form used in equation (23) can be used to generate approximations to  $f(t)$  that have arbitrary

accuracy. All that has to be done is to keep increasing the number of terms  $n$  and whenever this fails to increase the accuracy, then increase the separation parameter  $m$ . There are no cancellation problems due to the  $a_k$  becoming extremely large as happens when  $b_k = k \cdot b$ . The normal equations of the least squares process have matrices whose condition number increases with  $n$  but the rate of increase is very slow.

#### DISCUSSION

The following recommendations regarding the use of exponential approximations are based on the information in table II:

1. If execution time is very important use approximation D8.1.
2. Any programs for which execution time is not critically important that currently use approximations W4 or L11 should be changed to use approximation D12.1. This will reduce the error by two order of magnitude at the expense of a negligible increase in execution time. In fact, it was found when converting a particular program from L11 to D12.1 that the execution time was decreased. This was because during the recoding some compiler generated complex arithmetic was replaced by separate evaluation of real and imaginary parts.
3. New programs should use approximation D24.2. It gives full word length accuracy on short word length computers and takes less than twice as long to execute as D12.1.
4. Programs that currently use approximation J10 should only be converted to D12.1 if a considerable amount of future use of the program is anticipated. Approximation D12.1 is no faster than J10 and is only an order of magnitude more accurate.

In non-planar flow two incomplete modified Struve functions are required. They both use the same exponential approximation but the non-planar term has an extra variable of integration factor. This acts as a weight function on the error. As a consequence the exponential approximations described in this report introduce more error into the non-planar part of the kernel than into the planar part. This was not investigated in any detail. It is felt that it is not very important because all successful non-planar programs, such as the various doublet lattice programs, use very large panels so the kernel is either planar or is attenuated by distance.

The integrals  $F(s,r)$  and  $G(s,r)$  are integrated by merely substituting  $g(t)$ , defined by equation (23), for  $f(t)$ , in equations (10) or (11) and then integrating termwise. Thus, if  $s \geq 0$

$$F(s,r) = e^{-irs} \sum_{k=1}^n a_k e_k / (2^{k/m} b + ir) \quad (25)$$

$$G(s,r) = sF(s,r) - e^{-irs} \sum_{k=1}^n a_k e_k / (2^{k/m} b + ir)^2 \quad (26)$$

where

$$e_k = \exp(-2^{k/m} bs) \quad (27)$$

The exponential factors in equations (25) and (26) should be computed from equation (27) only if  $k < m$ . If  $k$  is greater than  $m$  then  $e_k$  should be computed from the recursion

$$e_k = (e_{k-m})^2 \quad (28)$$

Occasionally it is necessary to compute  $F(s,r)$  and  $G(s,r)$  for complex  $r$ . This occurs when the frequency  $\omega$  in equation (1) has an imaginary component. If  $\text{Im}\{r\} < 0$  then the integrals (10) and (11) exist and the sums (25) and (26) are valid approximations. A minor problem is that the error estimates given by the third column of table II may be too low because they are based on a search of the  $s$ - $r$  plane for real  $s$  and  $r$ . If  $\text{Im}\{r\} > 0$  then the integrals (10) and (11) do not exist. This is because the oscillations are damped and the integrals (10) and (11) usually represent integration over the subsonic wake. Even if  $\text{Im}\{r\} > 0$  the sums (25) and (26) exist. They are approximation to Abel sums of the divergent integrals (10) and (11). The Abel sum of an exponentially diverging integral is obtained by inserting a factor  $\exp(-\epsilon t^2)$  into the integrand and taking the limit as  $\epsilon$  approaches zero. If it can be shown on physical grounds that the integrals should exist then they are defined by their Abel sums.

#### CONCLUDING REMARKS

Several different methods for evaluating the incomplete modified Struve functions that occur in unsteady aerodynamics were investigated. Of the methods investigated it was found that an exponential approximation to the algebraic part of the defining integral followed by a closed form integration furnished the best compromise among accuracy, execution speed, and code maintainability. If the exponent spacing of the exponential approximation is either an arithmetic sequence, as suggested by Laschka, or a geometric sequence, as suggested by Jordan, then the number of exponential function evaluations required to evaluate the incomplete Struve functions is reduced. This same sort of spacing also simplifies the evaluation of the coefficients of the approximation if least squares are used. Of the two spacing sequences the geometric is much better. For either spacing sequence least squares provides an easily automated way of computing the coefficients,  $a_k$  and the sequence multiplier  $b$ . Approximations with coefficients computed by least squares are more accurate than those of the same order with coefficients computed by manual curve fitting.

In the paper a very limited class of exponential approximations was investigated, namely those with arithmetic and geometric spacing exponent sequences and with coefficients computed by least squares. It is possible that other sequences and schemes for computing the coefficients would give more accuracy. In particular using a minimax algorithm to generate the coefficients and exponent multiplier would



certainly give a small increase in accuracy. A program to implement a minimax algorithm is much harder to write and is much more expensive to execute than a least squares program. Furthermore the increase in accuracy would only be very slight. However if a minimax program were available it could be used to generate exponential approximations over subintervals of the positive real axis with no greater effort than is required to fit the whole axis. This is not true for least squares because of the integrals that have to be computed (the ones that contained quarter order Bessel functions). Splitting the interval into subintervals can lead to a large increase in accuracy with no increase in computing time. The only penalty is in program maintenance and development cost.

#### REFERENCES

<sup>1</sup>Watkins, C. E.; Woolston, D. S.; and Cunningham, H. J.: A Systematic Kernel Function Procedure for Determining Aerodynamic Forces on Oscillating or Steady Finite Wings at Subsonic Speeds. NACA TR R-48, June 1959.

<sup>2</sup>Morino, L.: Steady, Oscillatory, and Unsteady Subsonic and Supersonic Aerodynamics -- Production Version (SOUSSA Pl.1) Vol. 1 -- Theoretical Manual. NASA CR 159130, January 1980.

<sup>3</sup>Harder, R. L.; and Rodden, W. P.: Kernel Function for Nonplanar Oscillating Surfaces in Supersonic Flow. Journal of Aircraft, Vol. 8, Aug. 1971, pp. 677-679.

<sup>4</sup>Giesing, J. P.; Kalman, T. P.; and Rodden, W. P.: Subsonic Unsteady Aerodynamics for General Configurations. AFFDL-TR-75-5, Part 1, Vol. 1, November 1971.

<sup>5</sup>Laschka, B.: Interfering Lifting Surfaces in Subsonic Flow. Presented at 29th AGARD Structures and Materials Panel Meeting, Istanbul, Turkey, 1969.

<sup>6</sup>Jordan, P. F.: Numerical Evaluation of the Three-Dimension Harmonic Kernel. 2.Flugwiss.24(1976), Heft4, pp. 205-209.

<sup>7</sup>Erdeyli, et. al.: Table of Integral Transforms, Vol. 1. McGraw-Hill, New York, 1964.

<sup>8</sup>Handbook of Mathematical Functions with Formulas, Graphs, and Mathematical Tables, NBS Applied Math. series No. 55, edited by M. Abramowitz and I. Stegun. U.S. Dept. of Commerce, June 1964.

TABLE I

Exponent multiplier, b and coefficients,  $a_k$ , for several approximations to  $1-t/\sqrt{1+t^2}$  of the form indicated by equation (23).

#### Approximation D8.1

n = 8      m = 1      b = .035003907466  
 $a_1$  = .004329519485       $a_2$  = .001601370746  
 $a_3$  = .033195062769       $a_4$  = .098682301170  
 $a_5$  = .376739860841       $a_6$  = .822464185014  
 $a_7$  = -.380262739620       $a_8$  = .043400039240

#### Approximation D12.1

n = 12      m = 1      b = .009054814793  
 $a_1$  = .000319759140       $a_2$  = -.000055461471  
 $a_3$  = .002726074362       $a_4$  = .005749551566  
 $a_5$  = .031455895072       $a_6$  = .106031126212  
 $a_7$  = .406838011567       $a_8$  = .798112357155  
 $a_9$  = -.417749229098       $a_{10}$  = .077480713894  
 $a_{11}$  = -.012677284771       $a_{12}$  = .001787032960

#### Approximation D24.2

n = 24      m = 2      b = .005209230865  
 $a_1$  = .000305311497       $a_2$  = -.001412280807  
 $a_3$  = .003845227615       $a_4$  = -.007196572664  
 $a_5$  = .011385147609       $a_6$  = -.014763498650  
 $a_7$  = .018969114027       $a_8$  = -.019842326360  
 $a_9$  = .025618710871       $a_{10}$  = -.020313397232  
 $a_{11}$  = .036575115249       $a_{12}$  = -.010202806435  
 $a_{13}$  = .069407344423       $a_{14}$  = .037308217964  
 $a_{15}$  = .177803740980       $a_{16}$  = .198282197469  
 $a_{17}$  = .433959048197       $a_{18}$  = .354218469431  
 $a_{19}$  = .104676453558       $a_{20}$  = -.715978991168  
 $a_{21}$  = .407542943867       $a_{22}$  = -.104393578248  
 $a_{23}$  = .015398943987       $a_{24}$  = -.001192670868

#### Approximation D72.3

n = 72      m = 3      b = .000065986269  
 $a_1$  = .000000487572       $a_2$  = -.000003844799  
 $a_3$  = .000015710073       $a_4$  = -.000044143564  
 $a_5$  = .000096360019       $a_6$  = -.000174937155  
 $a_7$  = .000276395746       $a_8$  = -.000392188471  
 $a_9$  = .000511902333       $a_{10}$  = -.000625480027  
 $a_{11}$  = .000725938341       $a_{12}$  = -.000808476891  
 $a_{13}$  = .000872553959       $a_{14}$  = -.000917456689  
 $a_{15}$  = .000947455433       $a_{16}$  = -.000961741082  
 $a_{17}$  = .000968885391       $a_{18}$  = -.000962841735  
 $a_{19}$  = .000960418999       $a_{20}$  = -.000941494817  
 $a_{21}$  = .000943838490       $a_{22}$  = -.000912640747  
 $a_{23}$  = .000939494732       $a_{24}$  = -.000883200418  
 $a_{25}$  = .000971868480       $a_{26}$  = -.000847331705  
 $a_{27}$  = .001082186979       $a_{28}$  = -.000771912330  
 $a_{29}$  = .001357091273       $a_{30}$  = -.000556797879  
 $a_{31}$  = .001997471929       $a_{32}$  = .000067960260  
 $a_{33}$  = .003487618691       $a_{34}$  = .001801105035  
 $a_{35}$  = .007010443761       $a_{36}$  = .006406650025  
 $a_{37}$  = .015440810290       $a_{38}$  = .018199043007  
 $a_{39}$  = .035536908427       $a_{40}$  = .047032188464  
 $a_{41}$  = .081594062558       $a_{42}$  = .111356164158  
 $a_{43}$  = .174138343702       $a_{44}$  = .222492227365  
 $a_{45}$  = .288676153073       $a_{46}$  = .263088797407  
 $a_{47}$  = .143795607125       $a_{48}$  = -.194655408459  
 $a_{49}$  = -.414538285804       $a_{50}$  = -.093514761246  
 $a_{51}$  = .562053915950       $a_{52}$  = -.395454683729

$a_{53} = .132558644137$   $a_{54} = -.010481139795$   
 $a_{55} = -.022964836837$   $a_{56} = .027218864137$   
 $a_{57} = -.024548039318$   $a_{58} = .020804555835$   
 $a_{59} = -.017250853224$   $a_{60} = .014078375164$   
 $a_{61} = -.011265419745$   $a_{62} = .008772771052$   
 $a_{63} = -.006583208288$   $a_{64} = .004702560548$   
 $a_{65} = -.003149336650$   $a_{66} = .001939706215$   
 $a_{67} = -.001071671331$   $a_{68} = .000513691017$   
 $a_{69} = -.000203826307$   $a_{70} = .000062322287$   
 $a_{71} = -.000012950446$   $a_{72} = .000001360075$

TABLE II  
Properties of various approximations  
to  $1 - t/\sqrt{1+t^2}$ .

	max $ e(t) $	max $ E(s,r) $	time
W4	1.6E-3	2.3E-2	355
L11	1.3E-3	1.8E-2	382
D11	3.5E-4	2.6E-3	382
J10	1.3E-4	1.7E-3	407
D8.1	1.6E-4	1.1E-3	293
D12.1	2.5E-5	1.9E-4	411
D24.2	3.5E-7	2.1E-6	768
D72.3	3.0E-10	-----	2250

The first column of the table is the approximation designator.

The second column is the maximum error in the integrand approximation. It is very easy to compute but not too closely related to the error in the integral.

The third column is the maximum error in the integral for the planar component only. It is extremely expensive to compute.

The fourth column is the computer execution time for a single evaluation of the planar integral with positive lower limit and infinite upper limit. It is expressed as a multiple of the computer's add time.

#### APPENDIX

##### THE LEAST SQUARES PROCEDURE FOR COMPUTING COEFFICIENTS AND EXPONENTS

The function

$$f(t) = 1 - \frac{t}{\sqrt{1+t^2}} \quad (A1)$$

is to be approximated by an exponential sum

$$g(t) = \sum_{k=1}^n a_k \exp(-bp_k t) \quad (A2)$$

The number of terms,  $n$ , is preassigned as are the exponent coefficients  $p_k$ . Although the only  $p_k$  arrays for which calculations have been performed are  $p_k = k$  and  $p_k = 2^{k/m}$  the least squares procedure is valid for any preassigned  $p_k$  array. The only restriction is that all the  $p_k$  be distinct.

In the least squares procedure the coefficients  $a_k$  and the exponent  $b$  in equation (A2) are chosen to minimize the integral

$$E = \int_0^{\infty} w(t) [g(t) - f(t)]^2 dt \quad (A3)$$

There is no reason to suppose that this is an optimum choice for the  $a_k$  and  $b$ . In fact, there is some evidence the minimizing the maximum error  $|g(t) - f(t)|$  would be a better choice. However, minimizing  $E$  certainly gives a good set of coefficients and exponent and the process is very easy to automate. If the weight function  $w(t)$  in equation (A3) is set to 1 then the absolute value of the error function

$$|e(t)| = |g(t) - f(t)| \quad (A4)$$

takes on its maximum values near the ends of the approximation interval. The weight function

$$w(t) = (t-a)^{-1/2}(b-t)^{-1/2} \quad (A5)$$

is frequently used to make a least squares approximation over a finite interval  $(a,b)$  closely resemble a minimax approximation. In equation (A3)  $b = \infty$  and  $a = 0$  so the  $(b-t)^{-1/2}$  factor is undefined and the  $(t-a)^{-1/2}$  factor is

$$w(t) = t^{-1/2} \quad (A6)$$

Use of this weight function also makes some required integrals easier to evaluate.

The coefficients  $a_k$  and the exponent multiplier  $b$  are computed by setting  $\partial E / \partial a_k$  to zero for any value of  $b$  and by setting  $dE/db$  to zero where the  $a_k$  are functions of  $b$  defined by the condition  $\partial E / \partial a_k = 0$ .

$$\text{Let} \quad \frac{1}{2} \frac{\partial E}{\partial a_k} = 0 \quad (A7)$$

Then

$$\int_0^{\infty} t^{-1/2} [g(t) - f(t)] \exp(-bp_k t) dt = 0 \quad (A8)$$

That is

$$\begin{aligned} \sum_{k=1}^n a_k \int_0^{\infty} t^{-1/2} \exp[-b(p_k + p_k)t] dt \\ = \int_0^{\infty} t^{-1/2} \exp(-bp_k t) f(t) dt \end{aligned} \quad (A9)$$

The Laplace transform of  $t^{-1/2}$  is

$$\int_0^{\infty} e^{-pt} t^{-1/2} dt = \sqrt{\pi} p^{-1/2} \quad (A10)$$

so equation (A9) can be written

$$\sum_{k=0}^n c_{\ell k} a_k = d_{\ell} \quad (A11)$$

where

$$c_{\ell k} = (p_{\ell} + p_k)^{-1/2} \quad (A12)$$

$$d_{\ell} = \sqrt{(b/\pi)} H(bp_{\ell}/2) \quad (A13)$$

and

$$H(y) = \sqrt{\left(\frac{\pi}{2y}\right)} - \int_0^{\infty} e^{-2yt} t^{1/2} (1+t^2)^{-1/2} dt \quad (A14)$$

A closed form expression for  $H(y)$  is obtained by differentiating the Laplace transform pair 4.3(32) of ref. 7 and then exploiting some relationships between parabolic cylinder functions and Bessel functions, equations 19.3.7 and 19.15.9 of ref. 8. The expression is

$$H(y) = \pi \left(\frac{\pi y}{2}\right)^{1/2} [J_{1/4}(y) J_{-3/4}(y) - J_{-1/4}(y) J_{3/4}(y) + \sqrt{2} J_{1/4}(y) J_{3/4}(y)] \quad (A15)$$

After the  $a_k$  are computed then  $E$  can be evaluated as a function of  $b$ .

$$E = \int_0^{\infty} t^{-1/2} (g-f) g dt - \int_0^{\infty} t^{-1/2} (g-f) f dt \quad (A16)$$

The first integral in (A16) is zero because of equation (A8) so

$$E = E_0 - \sum_{k=1}^n a_k H(bp_k/2) \quad (A17)$$

where

$$E_0 = \int_0^{\infty} t^{-1/2} [f(t)]^2 dt \quad (A18)$$

This can also be integrated in closed form

$$E_0 = \frac{\pi}{\sqrt{2}} \left[ \frac{8\sqrt{2\pi}}{(\Gamma(1/4))^2} - 1 \right] \approx 1.16741087 \quad (A19)$$

The exponent  $b$  is obtained by solving  $dE/db = 0$

$$\frac{dE}{db} = - \sum_{k=1}^n [a'_k H(bp_k/2) + a_k (p_k/2) H'(bp_k/2)] \quad (A20)$$

where  $a'_k = da_k/db$  is obtained by differentiating equation (A11) and solving

$$\sum_{k=1}^n c_{\ell k} \frac{da_k}{db} = -\frac{1}{2\sqrt{(b/\pi)}} H\left(-\frac{bp_{\ell}}{2}\right) + \frac{p_{\ell}}{2} \sqrt{(b/\pi)} H'\left(-\frac{bp_{\ell}}{2}\right) \quad (A21)$$

and where

$$H'(y) = -\frac{1}{2y} H(y) + \sqrt{(\pi y/2)} \{J_{-3/4}^2(y) - J_{-1/4}^2(y) + J_{3/4}^2(y) - J_{1/4}^2(y) + \sqrt{2} [J_{-3/4}(y) J_{3/4}(y) + J_{1/4}(y) J_{-1/4}(y)]\} \quad (A22)$$

A detailed description of the algorithms used to implement the above equations follows:

I. Since  $E_0$  is independent of  $n$  and  $b$  it only has to be computed once. The quantity  $\Gamma(1/4)$  appearing in equation (A19) was computed by first using equations 6.1.48 of ref. 8 to compute  $\Gamma(145+1/4)$  and then using the functional equation for  $\Gamma(z)$ , equation 6.1.15 of ref. 8, to compute  $\Gamma(1/4)$ .

II. The number of terms,  $n$  is read into the program. The elements of the matrix  $C = [c_{\ell k}]$ , which are independent of  $b$ , are computed from equation (A12). Since  $C$  is symmetric only the diagonal and upper triangle of  $C$  are stored. The  $C$  matrix, which is positive definite, is factored without pivoting

$$C = LDU \quad (A23)$$

where  $L$  is a unit ( $\ell_{kk} = 1$ ) lower triangular matrix,  $D$  is a diagonal matrix, and  $U$  is a unit upper triangular matrix. Since  $L$  is the transpose of  $U$  only  $D$  and  $U$  are stored. They are overwritten onto  $C$  in memory. The algorithm dependent spectral norm condition number of  $C$ ,  $\max |d_{kk}| / \min |d_{kk}|$ , is also computed.

III. For each value of  $b$  both  $E(b)$  and  $E'(b) = dE/db$  are computed from equations (A17) and (A20). The  $a_k$  and  $a'_k$  are obtained by solving equations (A11) and (A20) using the LDU factorization described in step II above. The quantities  $H(y)$  and  $H'(y)$  for  $y = b \cdot p_k$ ,  $k=1$  to  $n$ , are computed from the four Bessel functions  $J_{-3/4}$ ,  $J_{-1/4}$ ,  $J_{1/4}$ , and  $J_{3/4}$ . These Bessel functions are computed using the Miller-Abramowitz algorithm described in example 1 of section 9.12 of ref. 7. The example is for integer order and uses equation 9.1.46 for normalization. Since  $J_{1/4}$ , etc. are of non-integer order equation 9.1.87 of ref. 7 has to be used for normalization. The highest argument gamma function in eq. 9.1.87 is computed as in Step I and the rest of the gamma functions are computed recursively from eq. 6.1.15.

IV. Finding a value of  $b$  for which  $E(b)$  is a minimum is performed in two steps.

A. A plot of  $\log_{10} E$  vs.  $\log_{10} b$  is constructed in order to determine the number of minima and their approximate locations.

B. Each approximate minimum is identified by three consecutive  $b$  values,  $b_1$ ,  $b_2$ , and  $b_3$ , for which the central value of  $E(b)$ ,  $E_2$  is lower than either of the two adjacent values,  $E_1$ , and  $E_3$ . These three values of  $b$  and the associated values of  $E'(b)$ ,  $E'_1$ ,  $E'_2$ , and  $E'_3$  are used as starters for Muller iteration which is used to solve the equation  $E'(b) = 0$ .

V. Step IV above determines many values of  $b$  for which  $E(b)$  is a relative minimum. For each of these values of  $b$  the maximum value of  $|e(t)|$  was obtained from a plot of  $e(t)$  vs  $t$ . The plot for which  $\max |e(t)|$  was a minimum gave the optimum value of  $b$ .

The program to implement the least squares process was originally written for  $p_k = k$ . For this choice of  $p_k$  array the  $C$ -matrix ( $c_{lk} = (l + k) - 1/2$ ) is extremely ill conditioned so all calculations were performed in double precision. Double precision is not needed for  $p_k = 2^k/m$  but was used because the program had already been written.

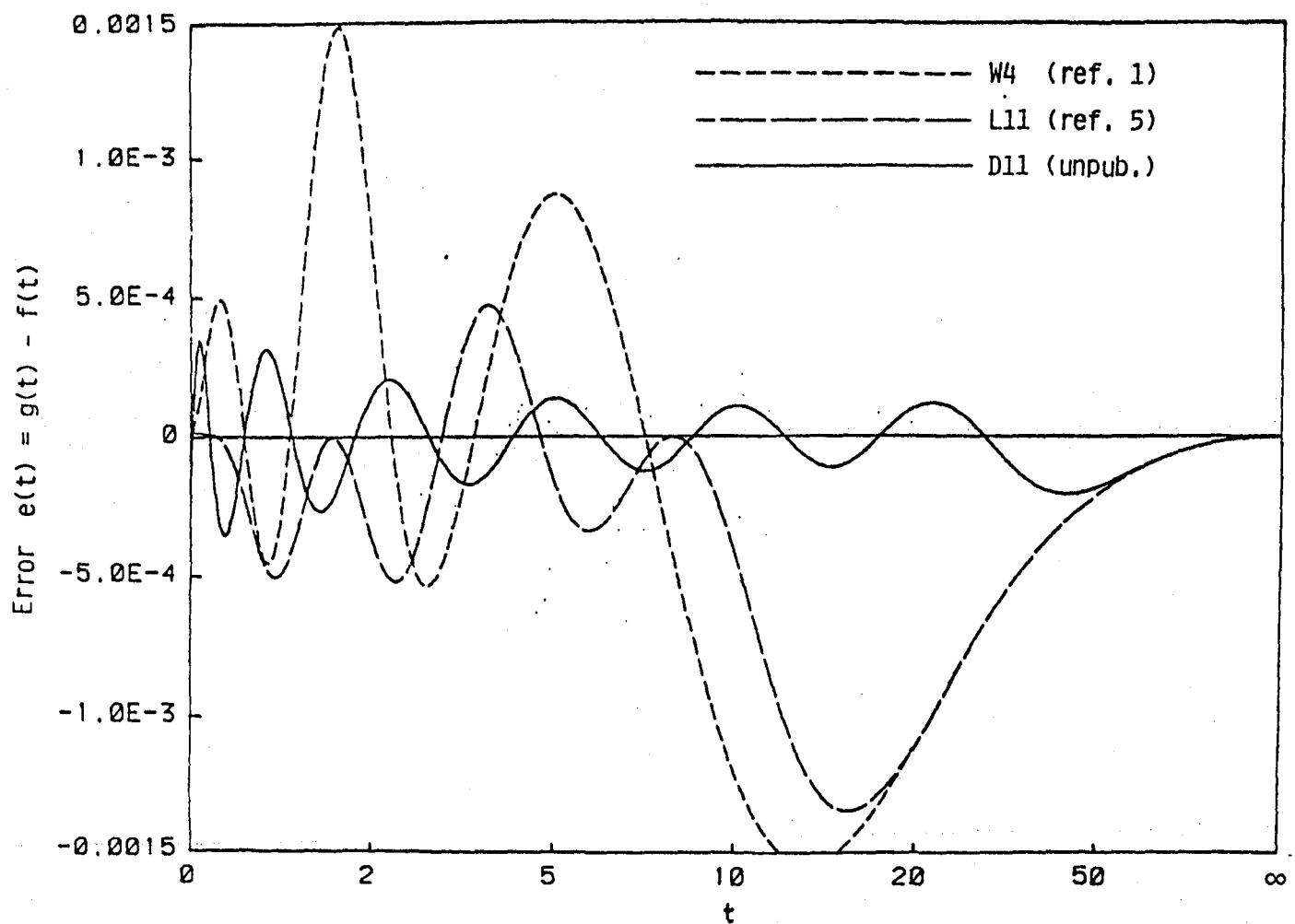


Figure 1. - Comparison of error in the exponential approximations W4, L11, and D11 to the function  $1-t/\sqrt{1+t^2}$ . The nonlinear t-scale on the plot results from mapping the  $(0, \infty)$  t-interval into a  $(-1,1)$  u-interval by the bilinear transformation  $u = (t+10)/(t-10)$ .

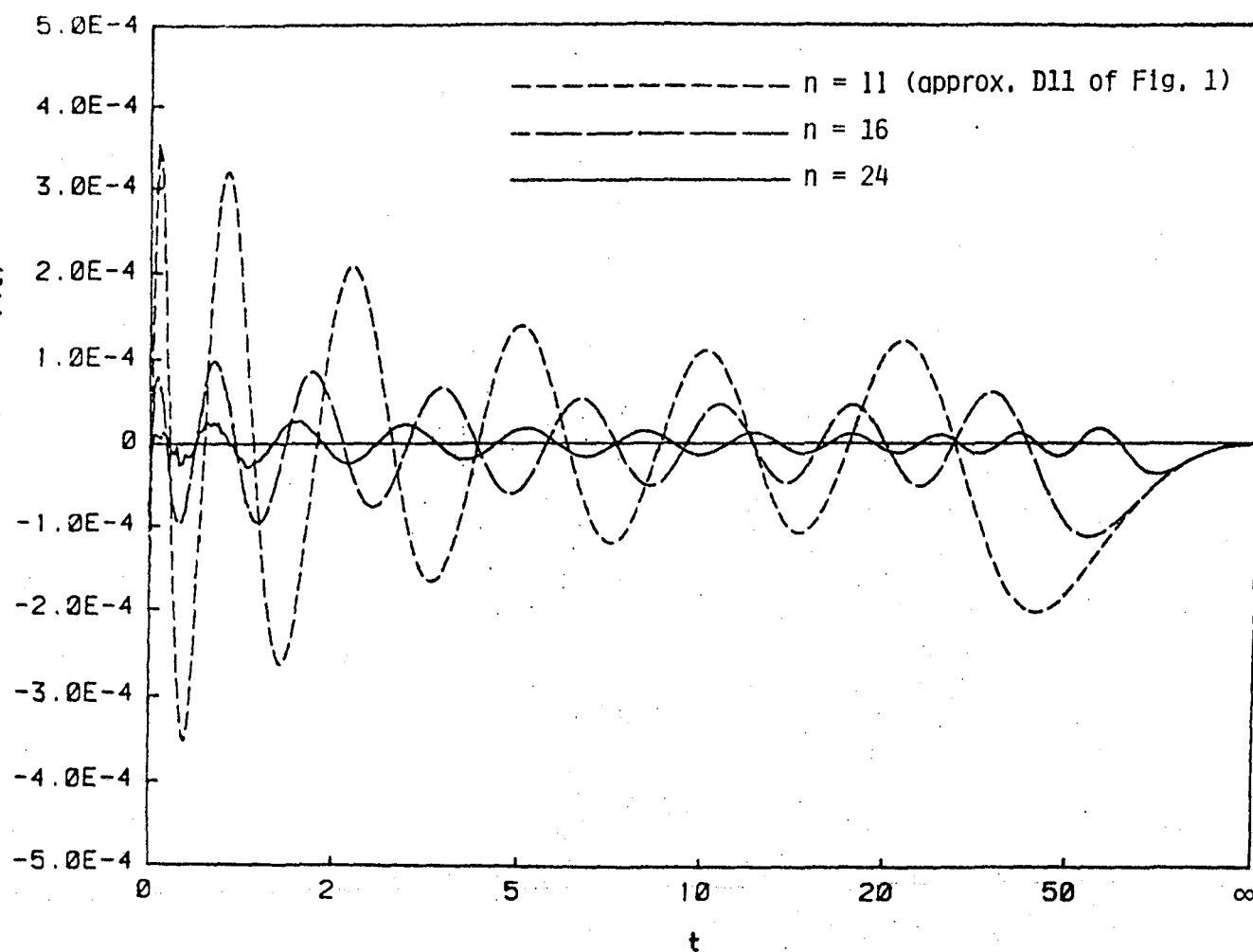


Figure 2. - Errors in least squares approximations for three values of  $n$  using Laschka's form for the exponents. Notice that the vertical scale is different from that of figure 1.

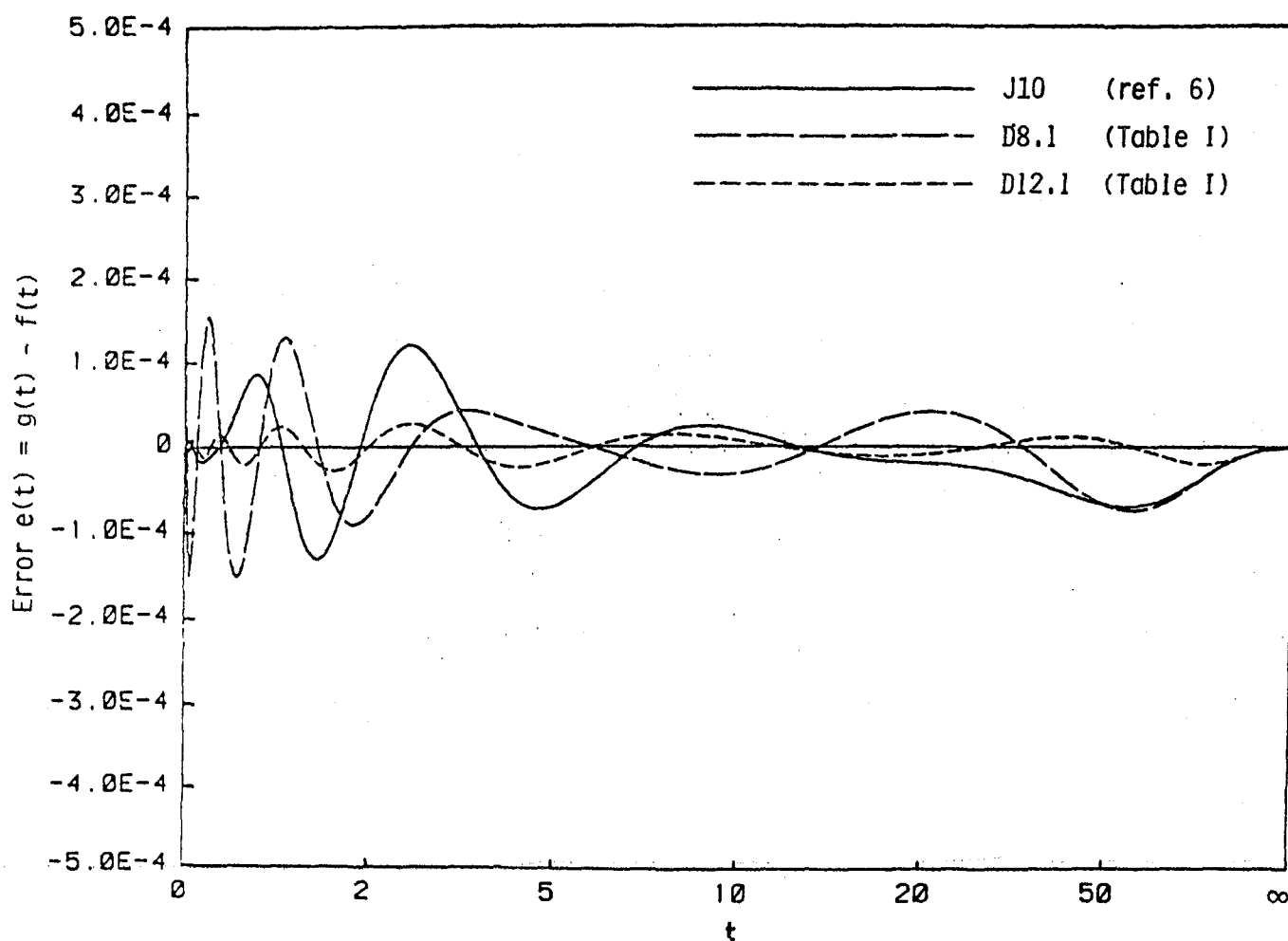


Figure 3. - Errors in least squares approximation using geometric exponent sequences. Even though  $\max |e(t)|$  is less for J10 than for D8.1 the latter is a better approximation because it has more nodes. (See  $E(s,r)$  in table II).







1. Report No. NASA TM 83281		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle AN ACCURATE METHOD FOR EVALUATING THE KERNEL OF THE INTEGRAL EQUATION RELATING LIFT TO DOWNWASH IN UNSTEADY POTENTIAL FLOW				5. Report Date April 1982	
				6. Performing Organization Code 2250	
7. Author(s) Robert N. Desmarais				8. Performing Organization Report No.	
9. Performing Organization Name and Address NASA Langley Research Center Hampton, VA 23665				10. Work Unit No. 505-33-53-07	
				11. Contract or Grant No.	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, DC 20546				13. Type of Report and Period Covered Technical Memorandum	
				14. Sponsoring Agency Code	
15. Supplementary Notes This paper was presented at the AIAA/ASME/ASCE/AHS 23rd Structures, Structural Dynamics and Materials Conference, May 10-12, 1982, New Orleans, Louisiana, AIAA Paper No. 82-687.					
16. Abstract This paper describes an accurate economical method for generating approximations to the kernel of the integral equation relating unsteady pressure to normalwash in nonplanar flow. The method is capable of generating approximations of arbitrary accuracy. It is based on approximating the algebraic part of the non elementary integrals in the kernel by exponential approximations and then integrating termwise. The exponent spacing in the approximation is a geometric sequence. The coefficients and exponent multiplier of the exponential approximation are computed by least squares so the method is completely automated. Exponential approximates generated in this manner are two orders of magnitude more accurate than the exponential approximation that is currently most often used for this purpose. Coefficients for 8, 12, 24, and 72 term approximations are tabulated in the report. Also, since the method is automated, it can be used to generate approximations to attain any desired trade-off between accuracy and computing cost.					
17. Key Words (Suggested by Author(s)) Flutter  Unsteady Aerodynamics			18. Distribution Statement Unclassified - Unlimited  Subject Category 02		
19. Security Classif. (of this report) Unclassified	20. Security Classif. (of this page) Unclassified	21. No. of Pages 14	22. Price A01		



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